Structures and Properties in Varying Phase Composition of PEO Coatings

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IBC Materials and Technologies, Inc. has developed a process for creating Plasma Electrolytic Oxidation (PEO) coatings on various aluminum alloy substrates. The purpose of the project was to understand the effects of IBC's proprietary process on the phase composition and mechanical properties of PEO coatings. The characterization was focused on the relationship between processing parameters and its effect on the alpha and gamma alumina volume fractions. Hardness, X-Ray Diffraction, and microscopy were performed to relate processing to properties.

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Project Background

PURDUE

Alpha phase aluminum oxide is preferred over gamma phase for many reasons. Alpha Al_2O_3 is much harder, thermodynamically stable, and more corrosion resistant. Conversely, gamma phase is thermodynamically unstable and has low surface energy [1]. To form alpha alumina requires a phase transformation from gamma phase at temperatures above 1000°C. PEO applies a high voltage of over 100 V to the metal sample which creates a plasma at the surface. An electrostatic attraction is created between the metal substrate and the oxygen in the electrolyte bath. This lowers the phase transformation temperature and assists the nucleation growth of alpha alumina [2].

Hardness	То
<u>Hardness</u>	test le
A fixed load of 100g and	+ L

ſop/Down	Cross Section	
load = 100g	test load = 50g	
	Diamond indenter adrangular pyramid)	

Conclusions

The mechanical properties of PEO coatings are primarily dependent on the phase fraction of alumina present. In understanding phase growth, the substrate composition, processing parameters, and nucleation must be considered.



Figure 1: Surface plasma interacting with metal sample in electrolyte baths [2].

50g were applied onto coating's surface the section and cross respectively. Random points on the surface and points along the the center of Cross section were evaluated.



Figure Micro-hardness indentation procedure using the Vickers method. Shown in red is the plastically deformed region which offsets data in close by indents.



Figure 5: Hardness of the cross section was found to be more indicative of the coating. No significant difference was found between IBC processes 1 and 2 with the exception being that process 1 samples had thicker coatings.

Cell Hardness Comparison

Hardness testing has shown that coating strength was unaffected by the different PEO processes provided. However, the cells display greater hardness than the surrounding wall. This suggests that the cells are comprised of greater amounts of alpha phase.

Cell size shows varying relationships with substrate alloying elements. Cell size increases between processes 1 and 2, also it increases with the substrate's copper content. Higher iron content within the substrate will decrease cell size.

Substrate dependence of the cell size may be due to iron and copper oxide nucleation. These inclusions provide a site for possible epitaxial growth through the coating [1][3].



Optical Microscopy

Cells were analyzed according to ASTM E-562 standards. Sets of 25 points were randomly chosen and counted for intersections and number of cells. This data was then used to calculate the areas.



volume fractions and cell Figure 2: Optical micrographs were overlaid with a 100 µm spaced grid at a random offset.



The transparent nature of the PEO coating allows for specialized microscopy. Optical micrographs taken under polarized light show a cellular structure (top) within the PEO coating. Evidence suggest that the cells grow columnar pattern а in (bottom). SEM testing from previous research shows

Location	Load (g)	Hardness (HV)	
Cells	50	1434 ± 65	
Cell wall	50	1266 ± 201	

Using the microscope attached to the microindenter, the cell structure was identified on the surface of the coating. A proper load and points were selected such that indents would be able to sample the cell structure. It was found that the cells are significantly harder than the outside wall structure. The results were confirmed using a 95% significance t-test.

X-Ray Diffraction



Figure 7: Cell radius is compared to the copper content within the substrate (left). Both IBC processes show and increase in the cell size as copper content increases. The iron content within the substrate alloy leads to a decrease in cell radius (right).

Recommendations

Further research should be focused on comparisons between phase composition and tribological properties. Scratch testing using a pin on disc method would be desired.





compared with substrate alloy grade and process parameter changes. A in change process and parameters an substrate increase in content alloy copper directly relate to larger Increased cells. iron content in the substrate alloy has a negative correlation with cell size.



Figure 6: XRD spectra for AI 7050 A identifying the multiple phases present with the coating. The presence of AI peaks representing the substrate indicates the entire thickness of the coating was analyzed.

Coating Properties				
Alloy Grade	alpha%	Hardness (HV)	Cell Radius (µm)	
AI 7050 A	6.5	1313	10.15	
AI 7050 B	0.0	1300	7.19	
AI 7075 C	2.7	1432	7.72	
AI 7075 D	41.4	1248	5.69	
AI C355 C83 E	89.6	1524	9.16	
AI C355 C97 F	0.2	1487	6.41	

References

[1] - Andersson, J. M. (2005). *Controlling the* Formation and Stability of Alumina Phases. Linköping, Sweden: Linköping: Linköpings Universitet.

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[3] - Wenbin X., Zhiwei D., Ruyi C., Tonghe Z. (2006). Growth regularity of ceramic coatings formed by *microarc oxidation on AI–Cu–Mg alloy*. Thin Solid Films.

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